

THERMOPHYSICAL CHARACTERIZATION OF THE HETEROGENEOUS SUBSURFACE AND APPLICATIONS

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6 Universities
1 Government Agency
45 Participants

Terrestrial Subsurface Thermal Regime

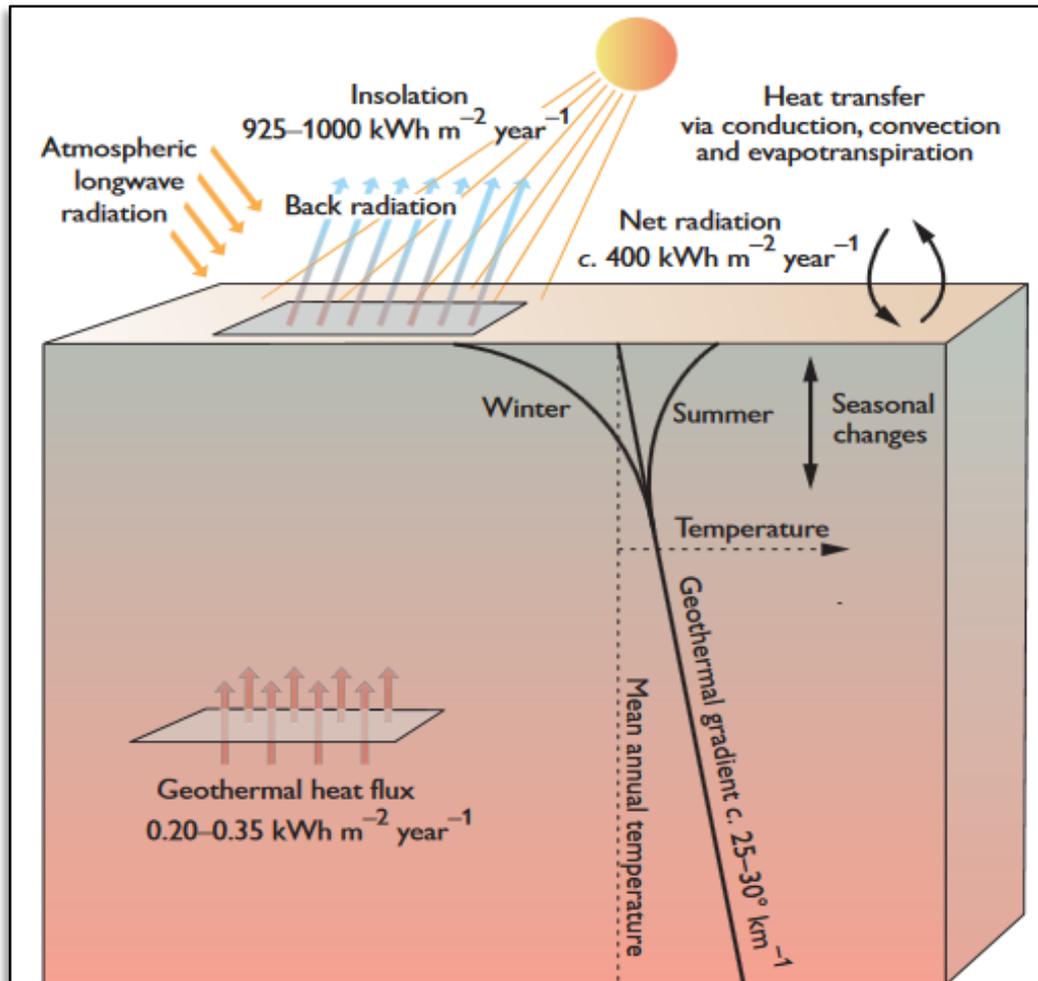
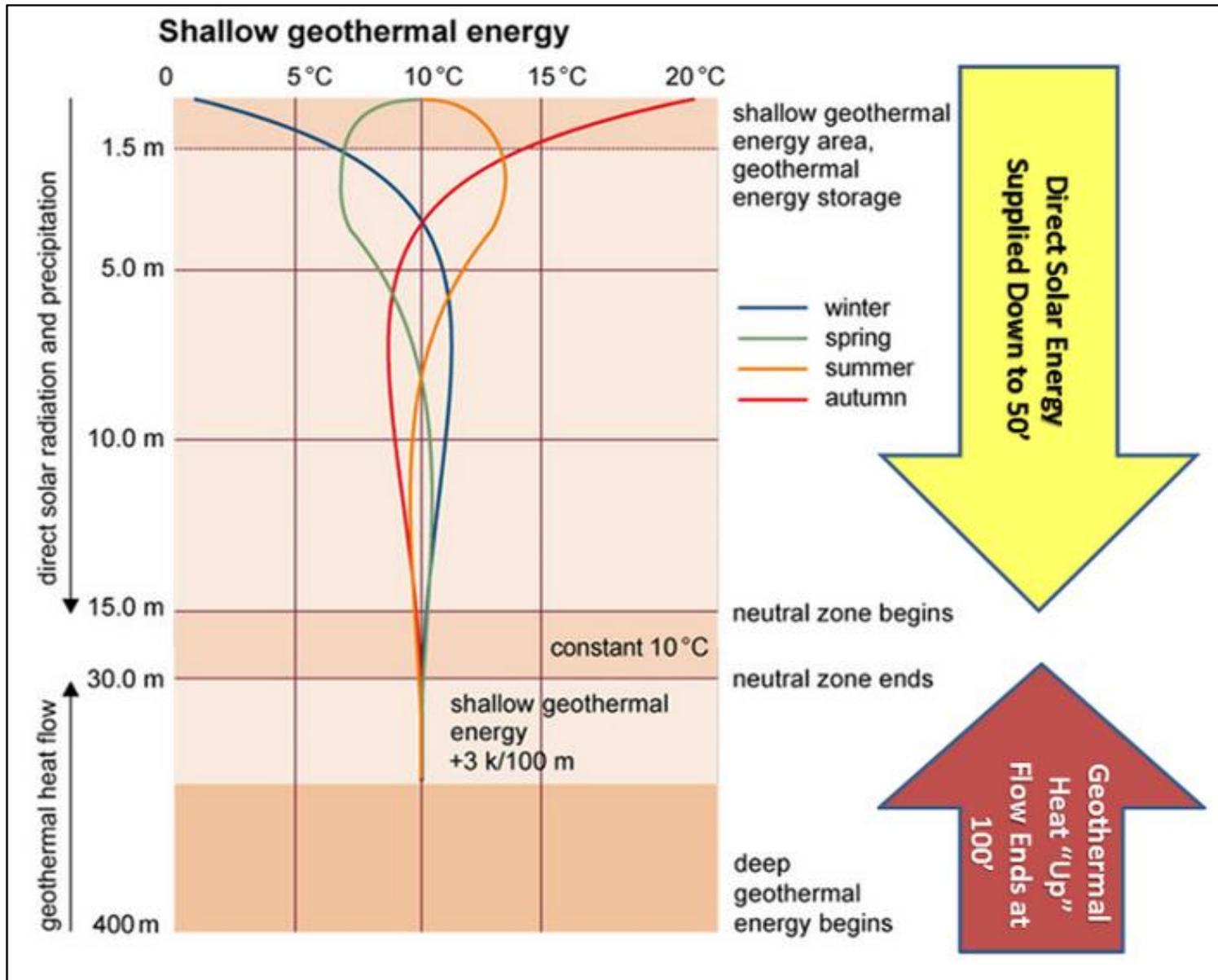


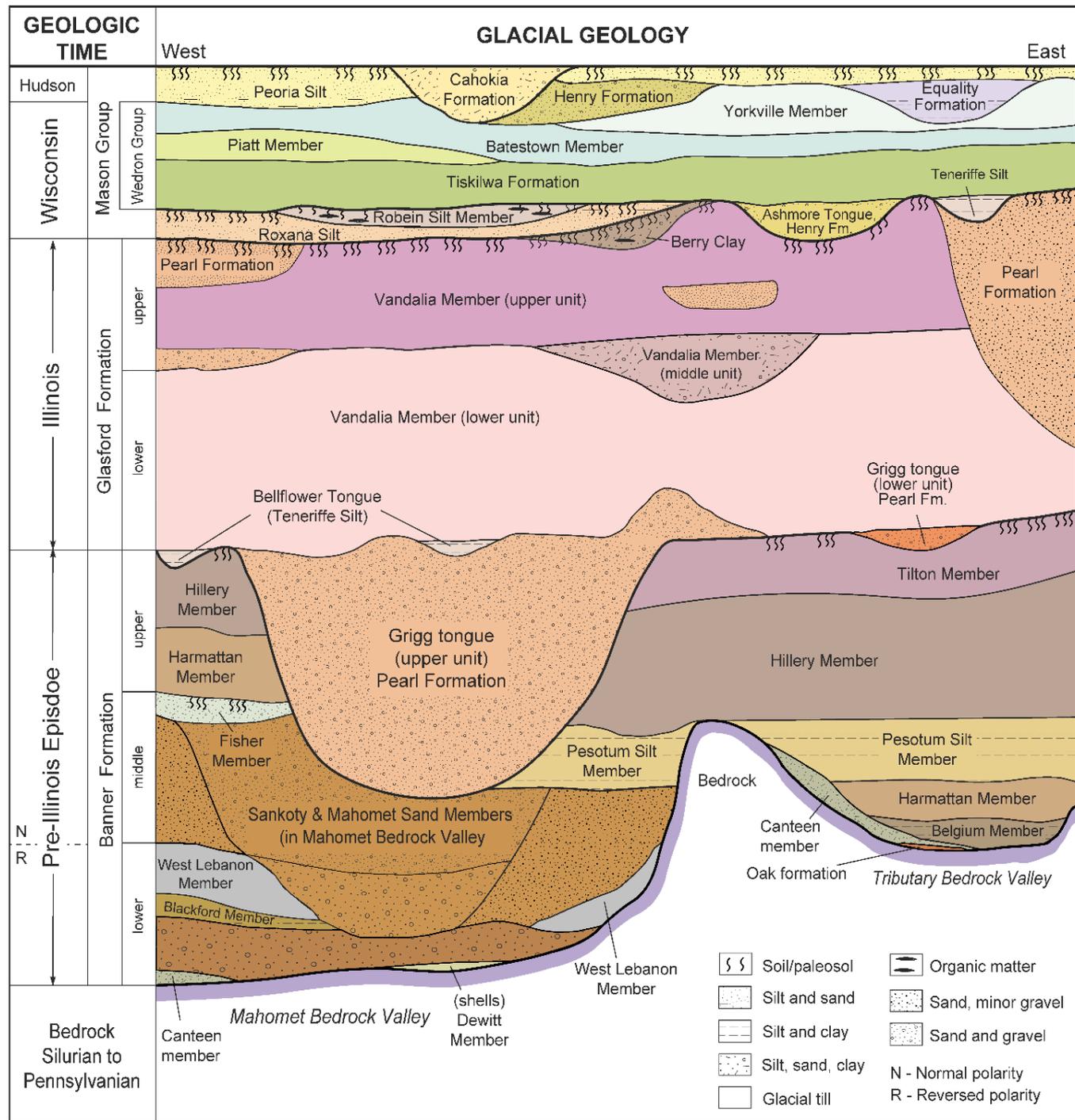
Fig. 1. Schematic block diagram showing the geothermal gradient and magnitude of geothermal heat flux and insolation with average values for Denmark as well as the seasonal zone of fluctuation in temperature (modified from Banks 2008).

Terrestrial Subsurface Thermal Regime



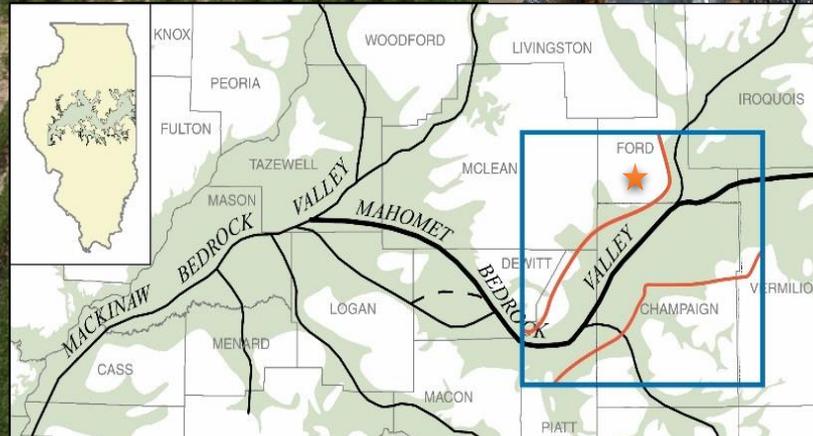
Geology and Hydrogeology Framework

Glacial systems are inherently heterogeneous

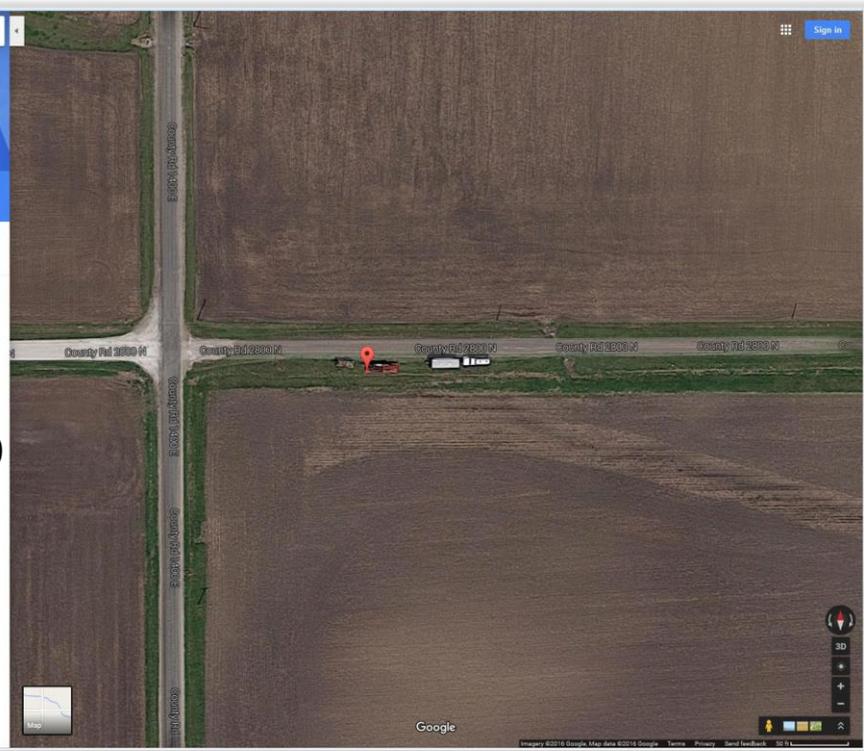
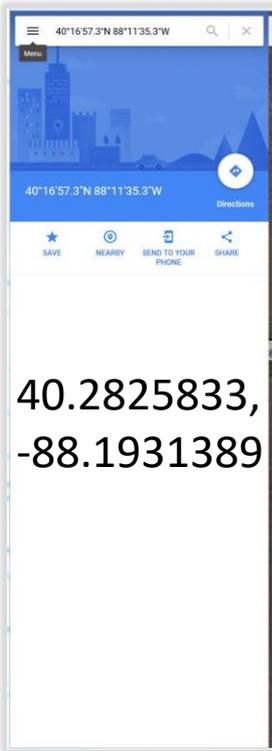




Critical Zone Observatory for Intensively Managed Landscapes (IML-CZO)



West Rantoul

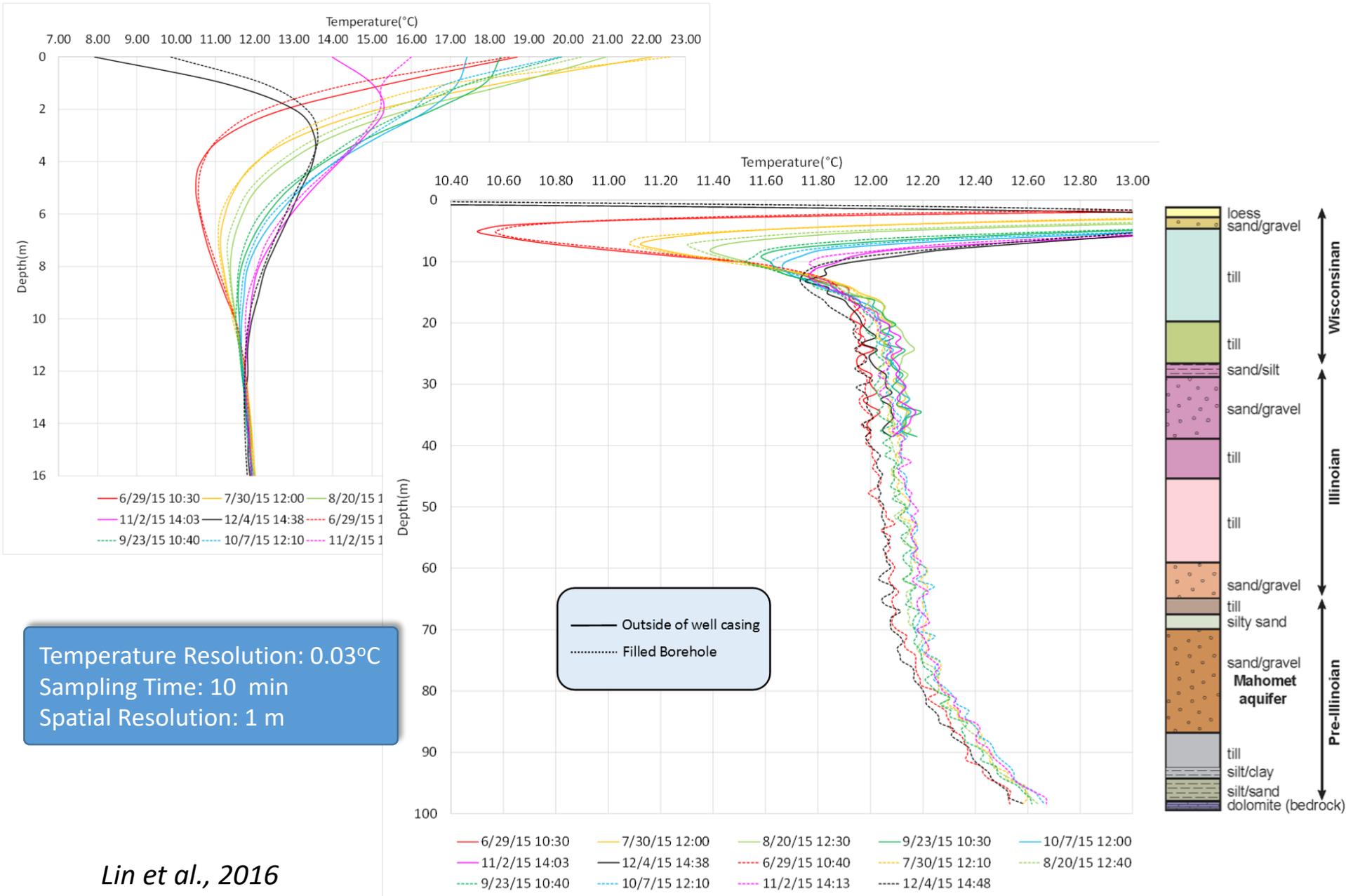


40-m well screened in Glasford aquifer



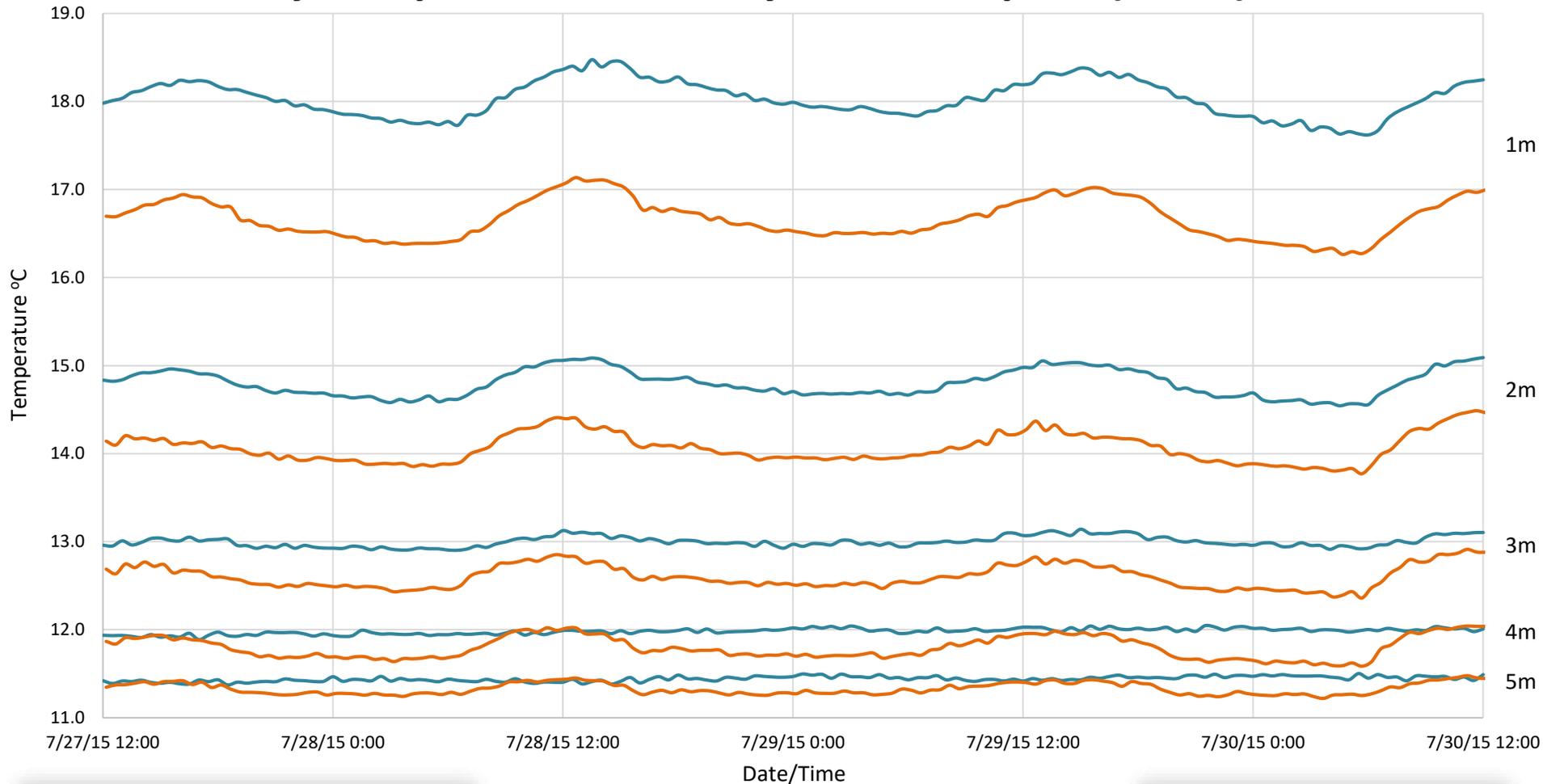
100-m hole penetrating Mahomet aquifer

Monthly Temperature Comparison from June-December, 2015



Semi-hourly Temperature at Every Meter Depths (1-5m)

— 40m Well
— 100m Hole



Semi-hourly summer temperatures at 1-meter depths (1–5 meters) reflect amplitude attenuation and phase shifts as heat is conducted in the subsurface.



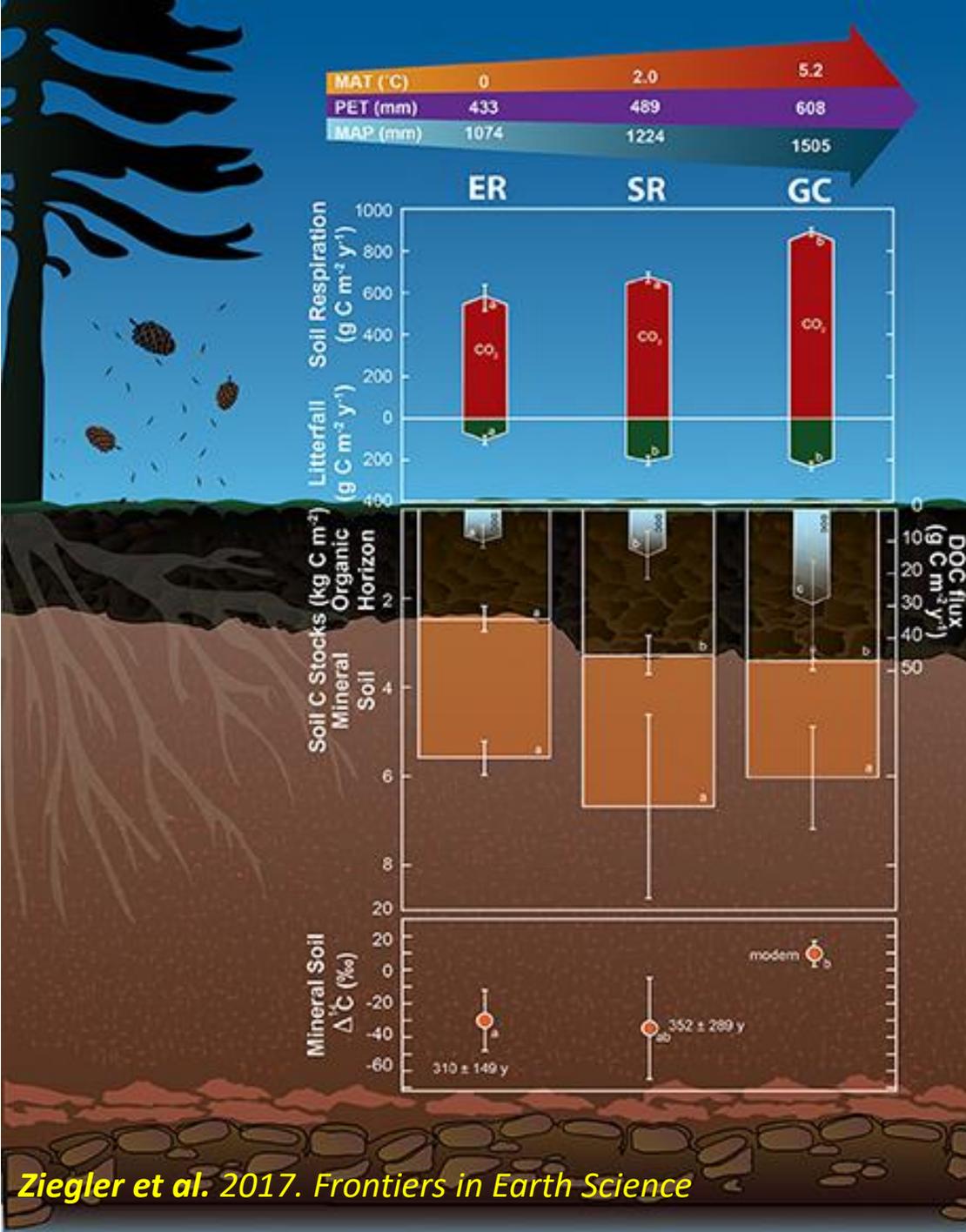
Lin et al., 2015

The preliminary results indicate:

- The derivative of the subsurface temperature alone depth corresponds to the hydrostratigraphic characterization and groundwater flow.
- A well might act as a temperature buffer to potentially interfere with the natural geothermal regime.



A regional rule-of-thumb temperature gradient of 1 °F/100 ft and an annual average temperature of 62 °F (16.6 °C) at 100 ft (30.5 m) below surface based on 40 years of observations and measurements in the Illinois Basin. (Frailey et al., 2004).



Short- and Long-Term Temperature Sensitivity in the Subsurface

Shallow Critical Zone

↑ Temperature and ↑ Precipitation



- ↑ Soil respiration by ~55%
- ↑ DOC fluxes to the mineral horizons by 300%
- ↑ Mobilization and subsequent loss of soil C

Deep Critical Zone?

Thermophysical and Hydrogeological Characterization??

Climate Change and Anthropogenic Influence

- Vertical Temperature Profiling with Climate Changes



- Well Interference
- Agriculture Influence
- Energy

Thermal Analysis for Geothermal Energy Alternatives 2016-2017

USDOE

- > 66% electrical energy and > 40% of natural gas is consumed in a building's utilities in US.
- In residential and commercial buildings, space heating and cooling consume 47% of the electrical power, and water heating accounts for an additional 12%.



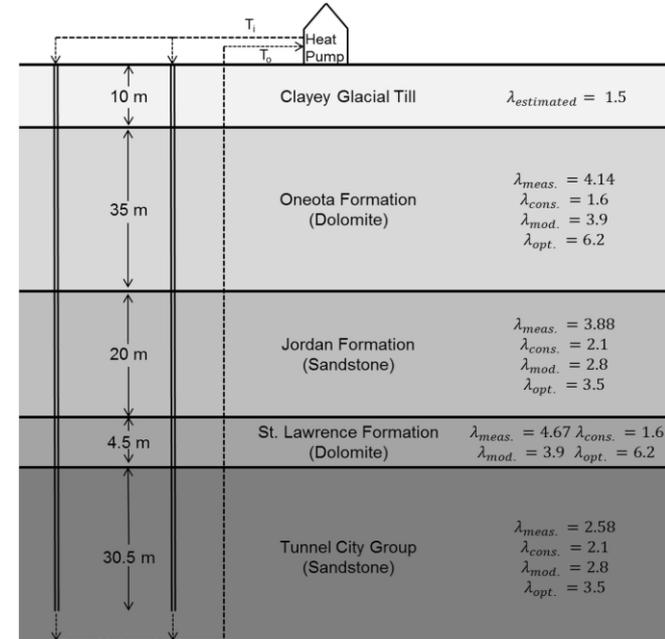
USEPA

Reduce energy consumption by up to:

- 44% compared with air-source heat pumps
- 72% compared with conventional electrical heating and air conditioning

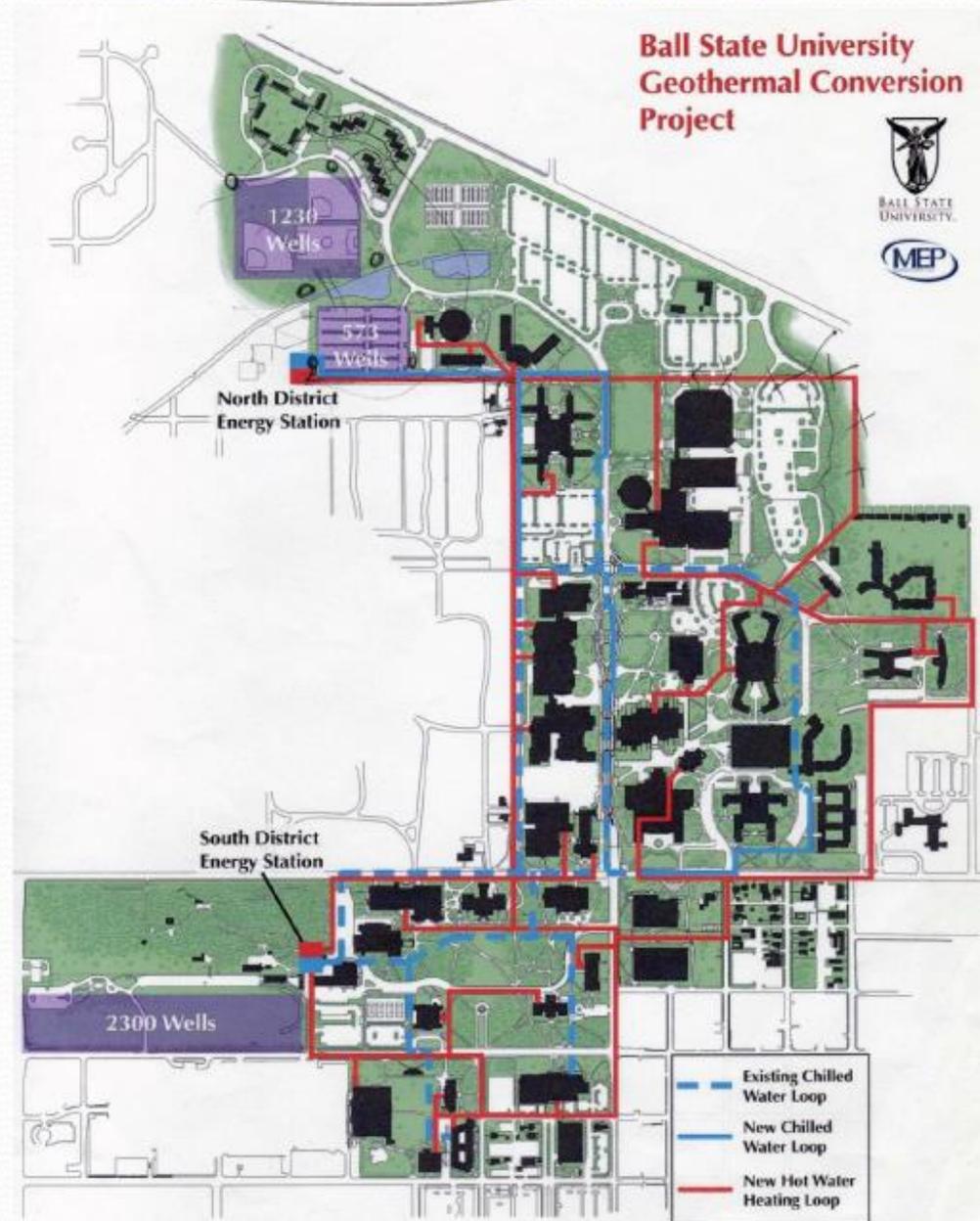
USDOD

Long-term solution on resource reliance and disaster reduction, such as reducing the number of hydraulic power dams for flood reduction.



BSU Geothermal Conversion

- Divided into two Phases, Phase I and Phase II
- Both phases are completed and running
- This study concerns the ground temperatures in Phase II since thermal loading began

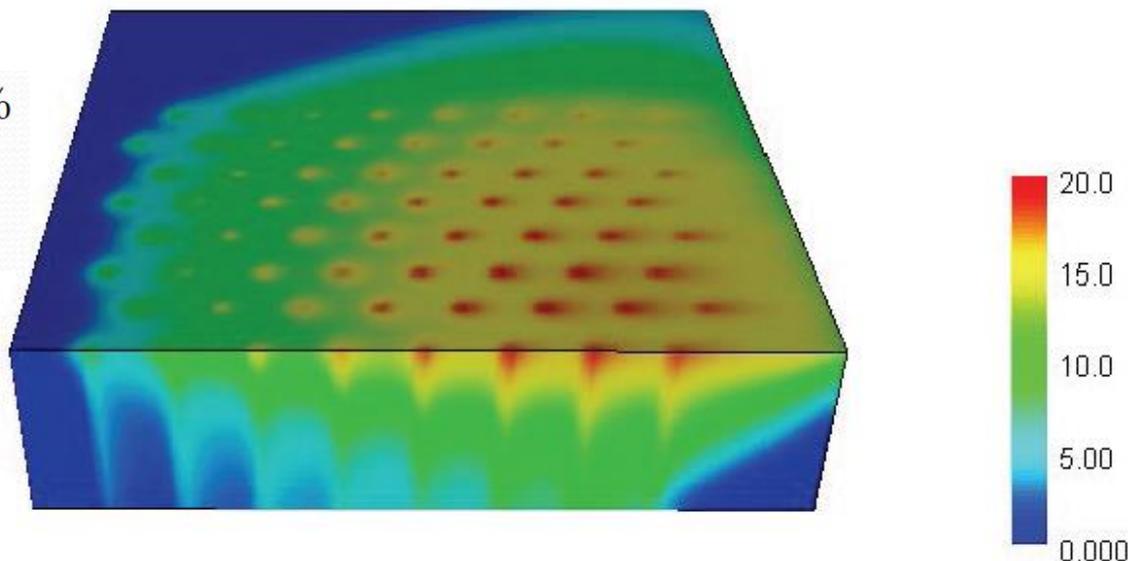


Advection & buoyant convection of thermal plume

- Preliminary data indicate that the BSU is in a thermal excess condition that provides thermal loading to the ground.
- In such conditions, excess thermal load may create a plume of warm buoyant groundwater that advects in the direction of groundwater flow.

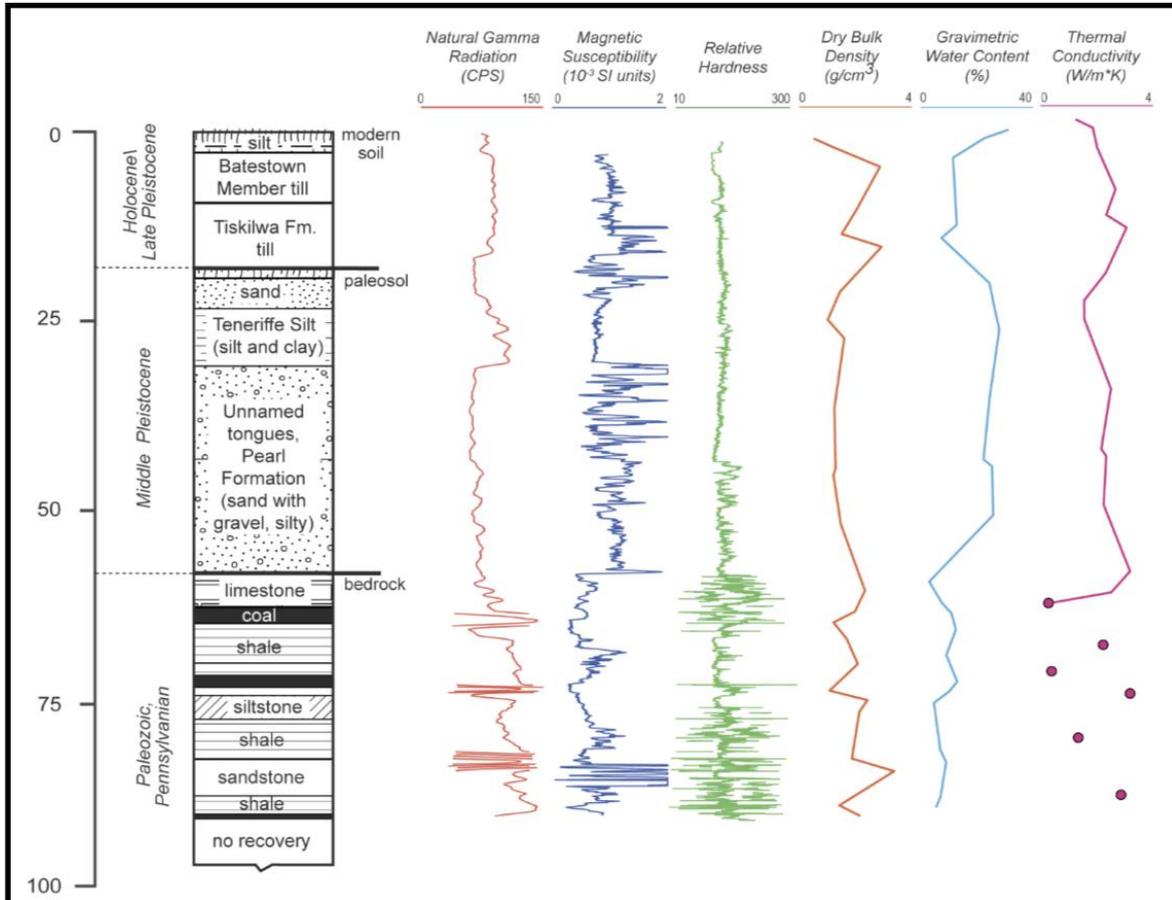
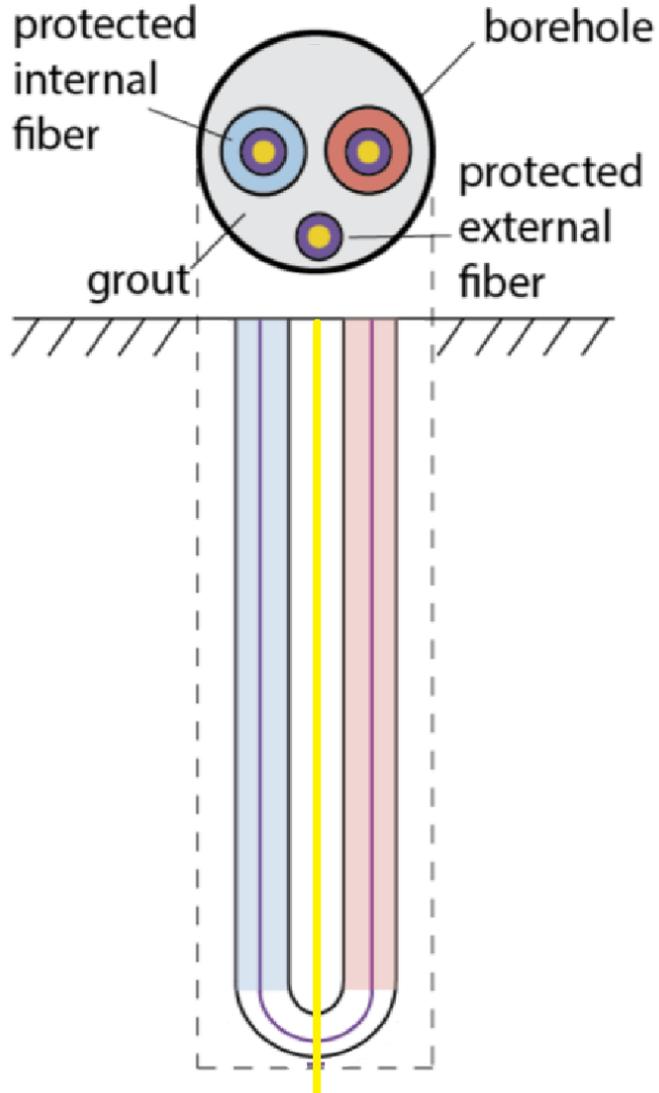
- ▶ Reduce carbon footprint by 50%
- ▶ Save \$2 million annually

Lowe et al. 2010

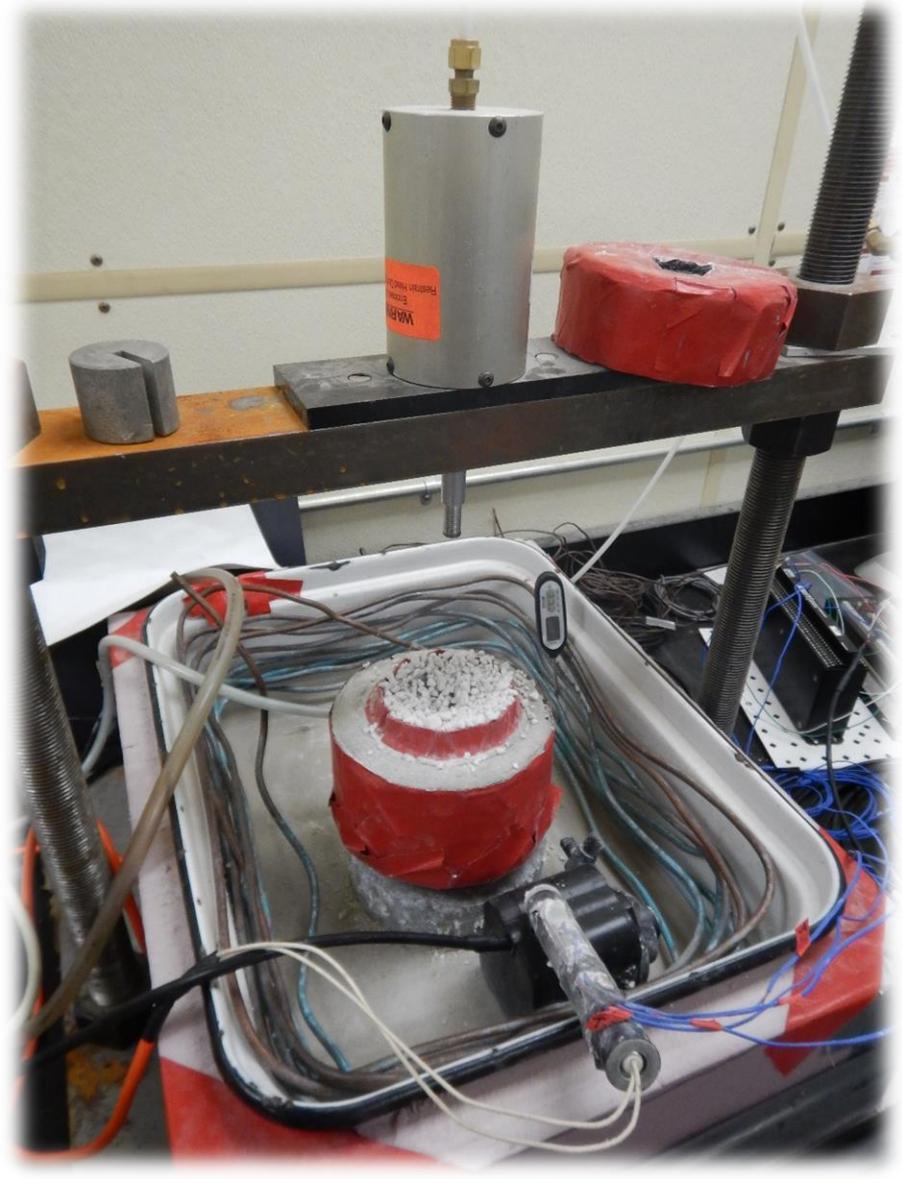
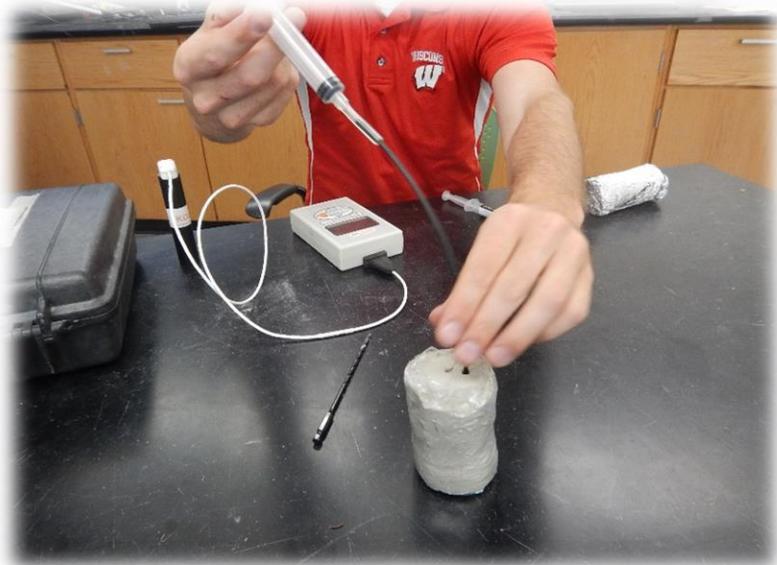


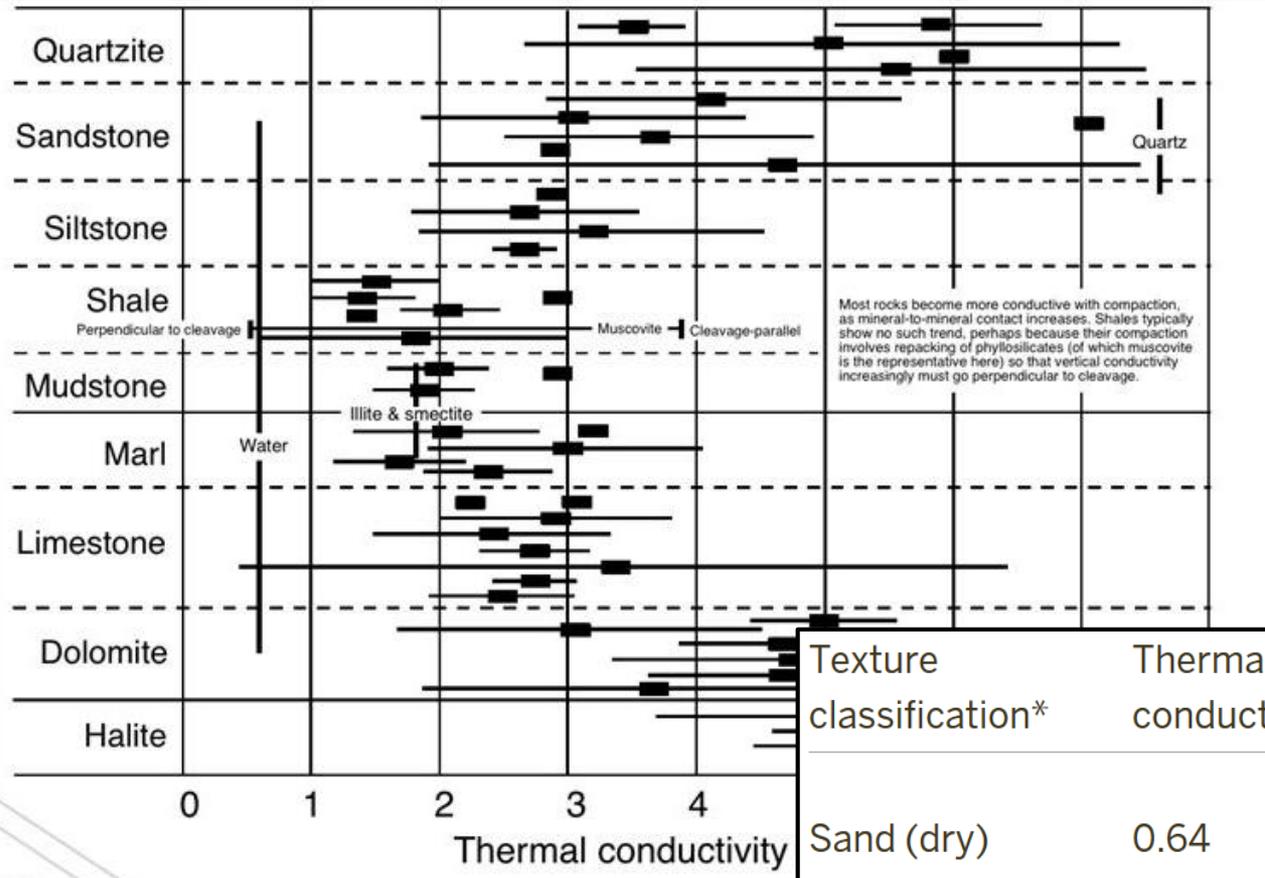
Courtesy of Mike Sukop

Geothermal Monitoring



Geothermal Property Analysis





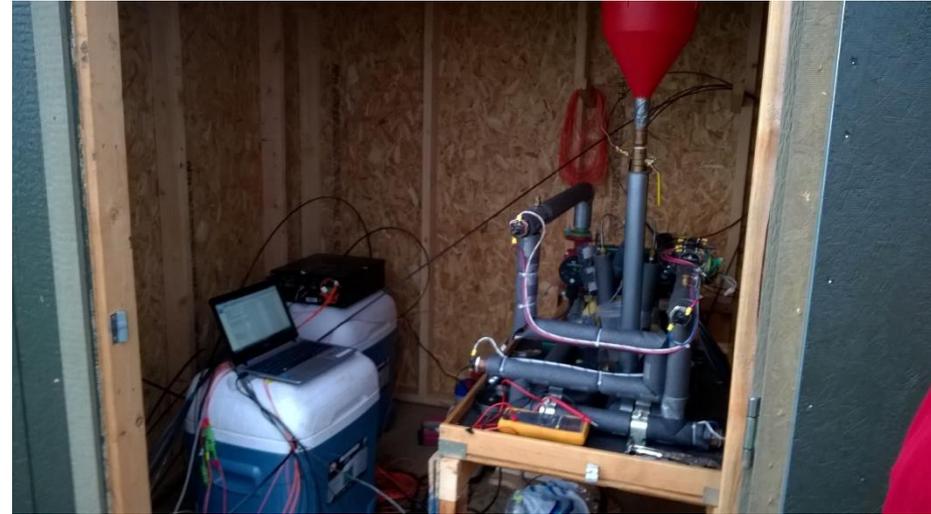
Moisture content ↑
 Thermal conductivity ↑
 Sandy sediments (↔)
 Clayey sediment (→←)

**What about bulk density,
 hardness,
 mineralogy, cementation,
 and flowing water?**

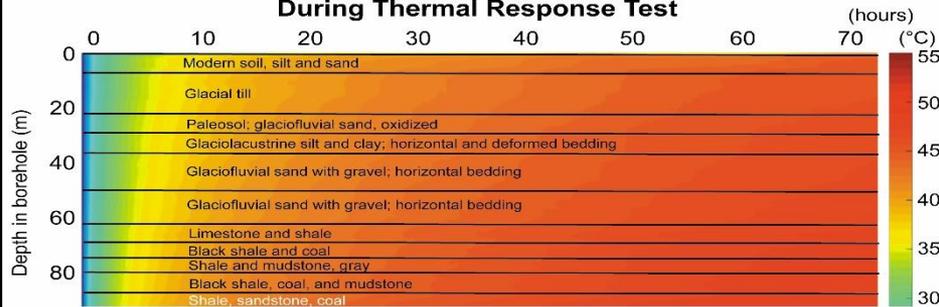
Texture classification*	Thermal conductivity (W/m*K)	Thermal diffusivity D (mm ² /s)
Sand (dry)	0.64	0.67
Sand (moist)	1.39	0.73
Silt loam (moist)	1.59	0.70
Silt loam (wet)	1.59	0.56
Clay loam (moist)	1.90	0.57
Clay loam (wet)	2.14	0.61

*Moisture contents are based on degree of saturation (dry: 0-25%, moist: 26-50%, wet: 51-99%)

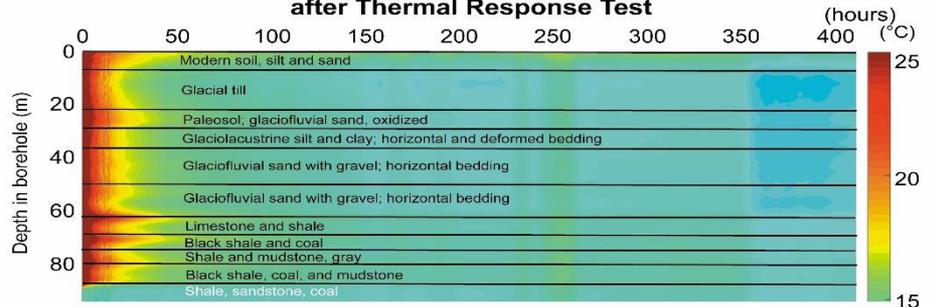
Distributed Thermal Response Test (DTRT)



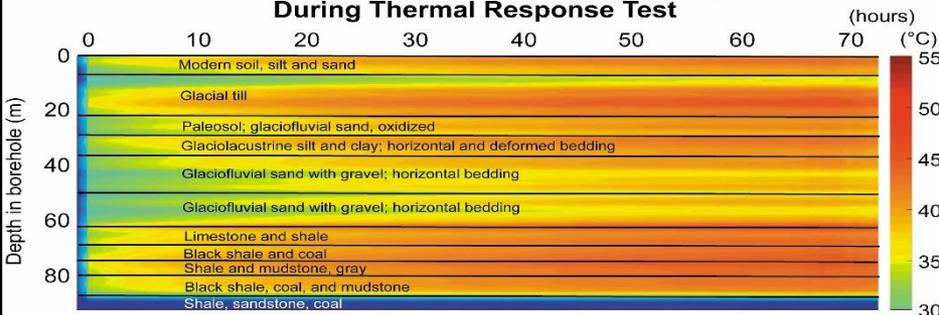
Temperature Inside Geothermal Loop During Thermal Response Test



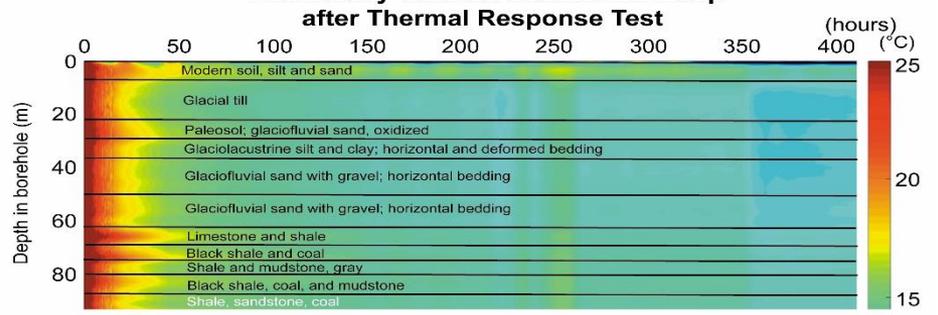
Heat Decay Inside Geothermal Loop after Thermal Response Test



Temperature Outside Geothermal Loop During Thermal Response Test

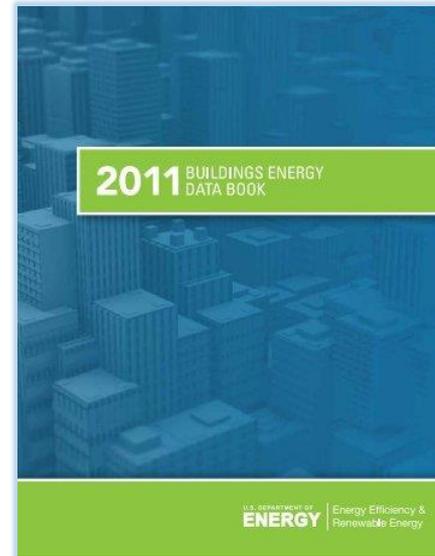


Heat Decay Outside Geothermal Loop after Thermal Response Test

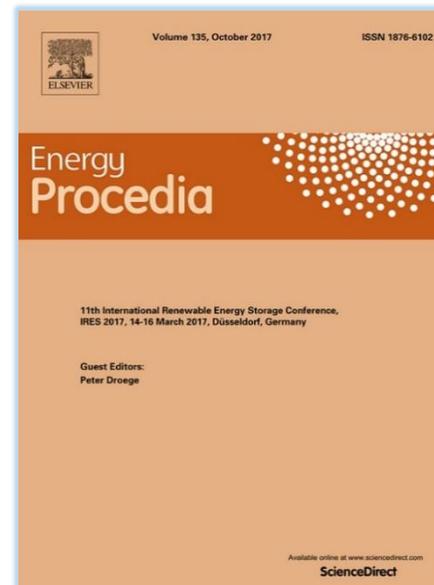


Greenhouse gas emissions from powering buildings

1. Heating, ventilation and cooling of buildings ~30% of global GHG
(IEA, 2016)
2. Heating and cooling (USA):
 - 47% of energy demand
(US DOE, 2012)
3. Energy usage in buildings (China):
 - 20% of total energy in China in 2012
 - 16% of total global energy use in 2012
(IEA, 2015)



The book is a compendium of statistics on residential and commercial building energy consumption



Geological Sequestration

The ISGS has completed several projects to study storing CO₂ deep underground

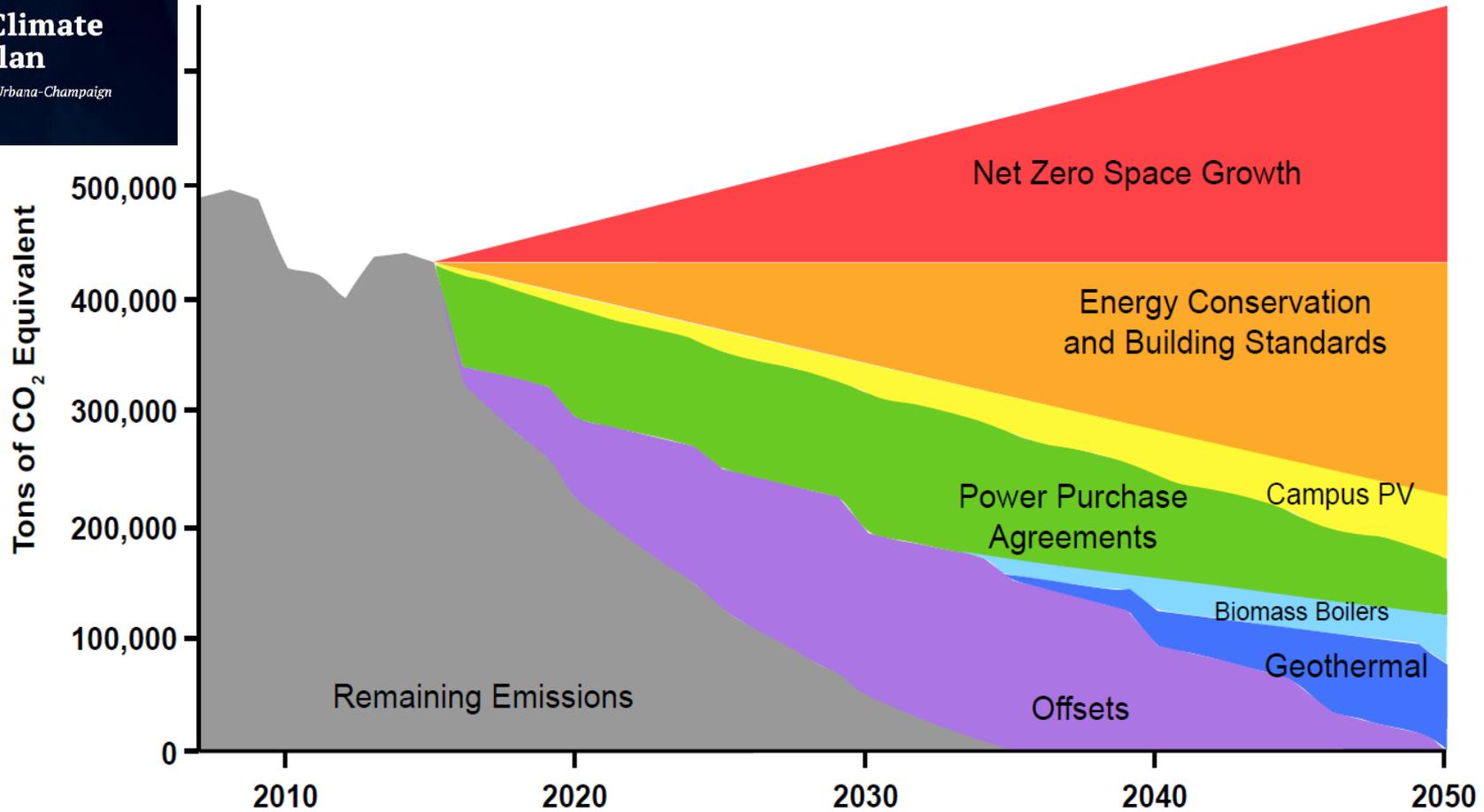


Figure 3: 2015 iCAP Wedge Diagram showing only energy emissions projected, with potential clean energy scenario



~ SPEC ~
Temperature Resolution: 0.01°C
Operating Temperature: -40°C ~ 65°C
Temporal Resolution: 15 sec
Temporal Range: Limited by Storage
Spatial Resolution: 1 m
Spatial Range: 5 km per channel
Number of Channels: 4

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Prairie Research Institute
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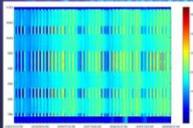
Dr. Richard C. Berg
State Geologist, ISGS Director



**Fiber-Optic
Distributed
Temperature
Sensing**

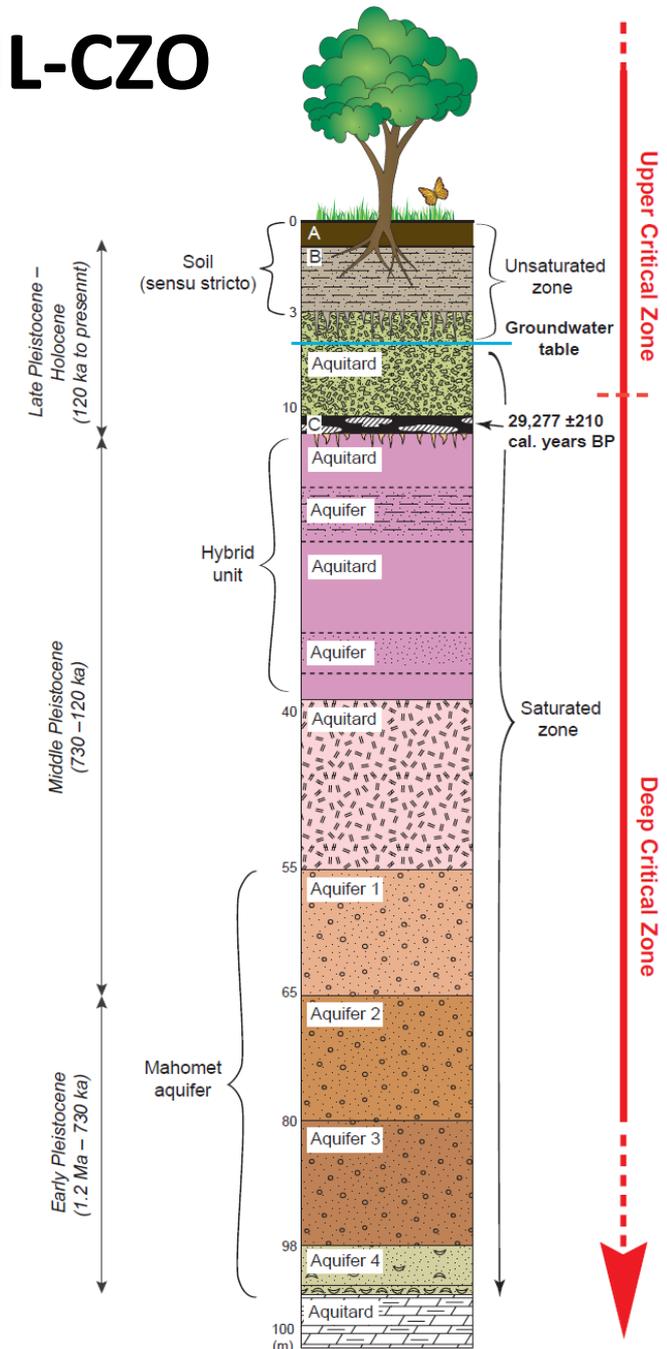
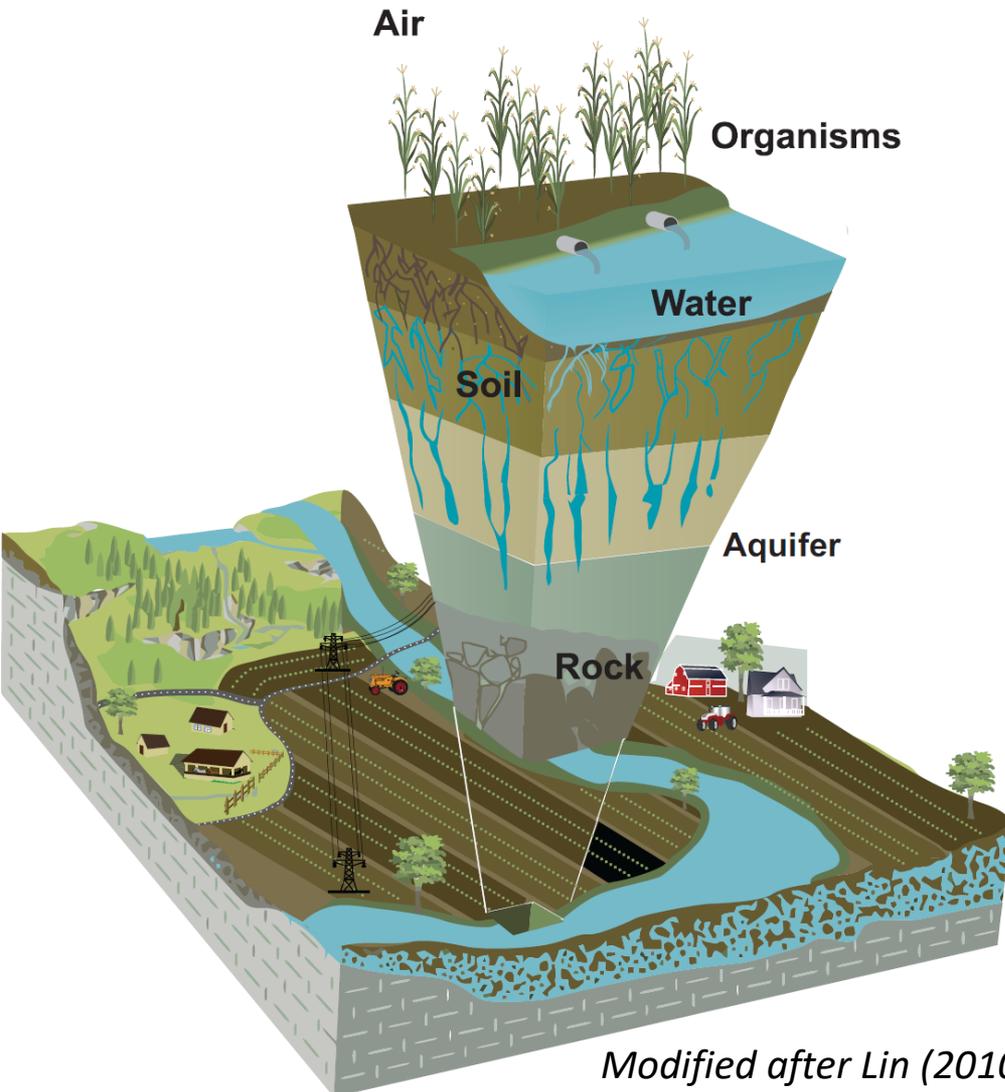
FO-DTS
@ ISGS

Measuring Illinois' Vital Signs

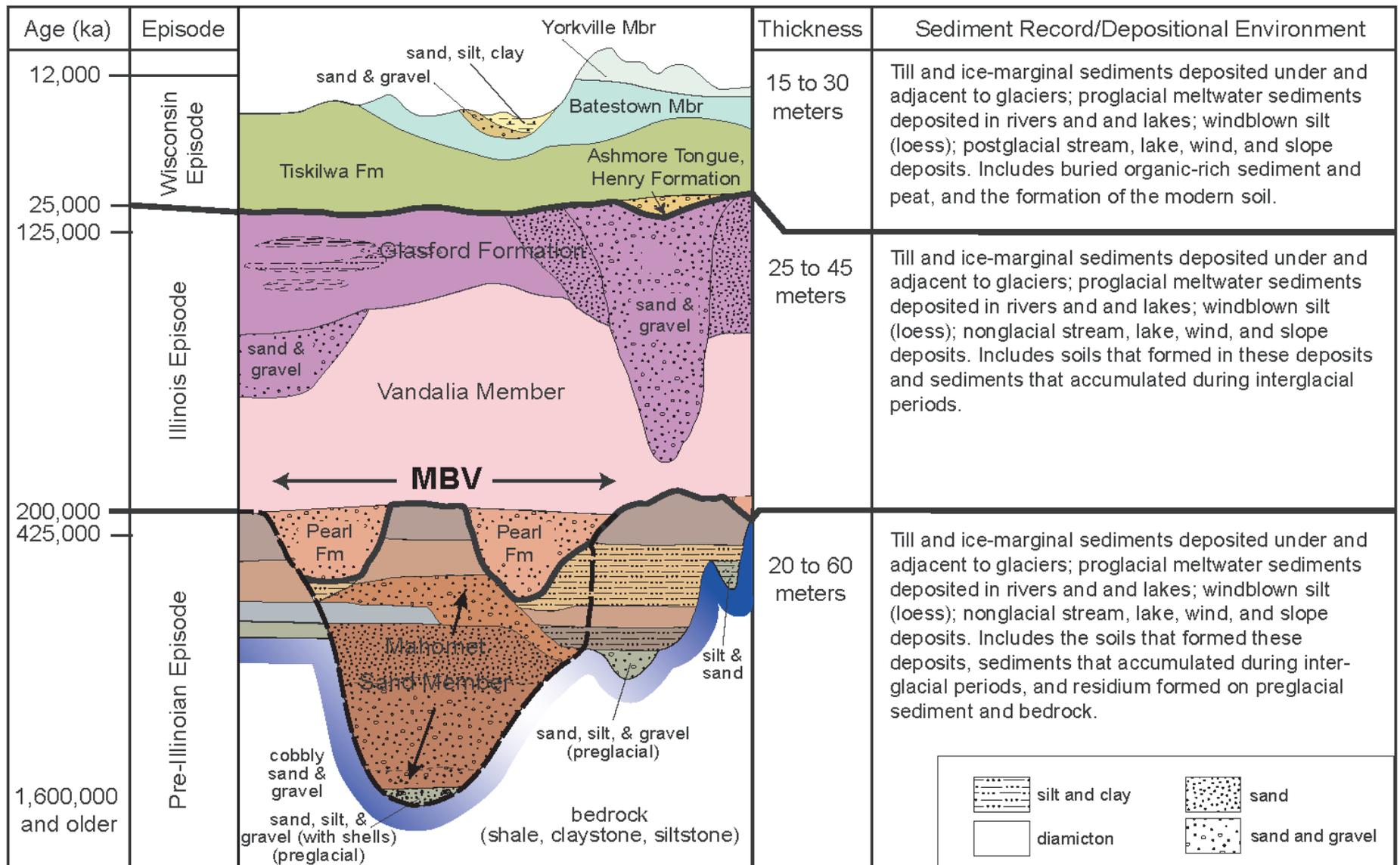


Upper Sangamon River Basin @ IML-CZO

including the modern soil, glacial sediment, the unsaturated zone, the saturated zone, and bedrock.

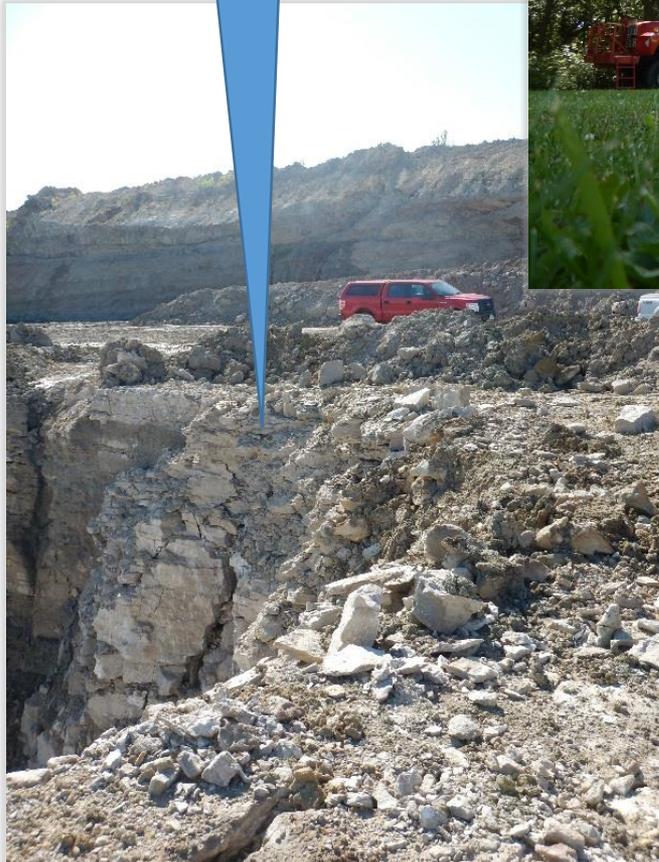


Modified after Lin (2010) and Akob and Küsel (2011)



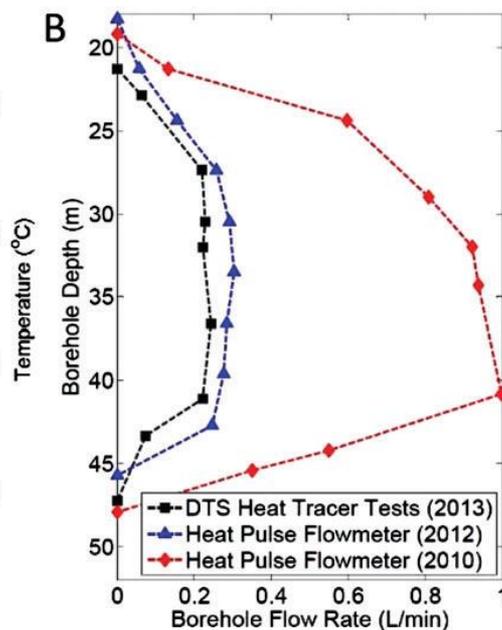
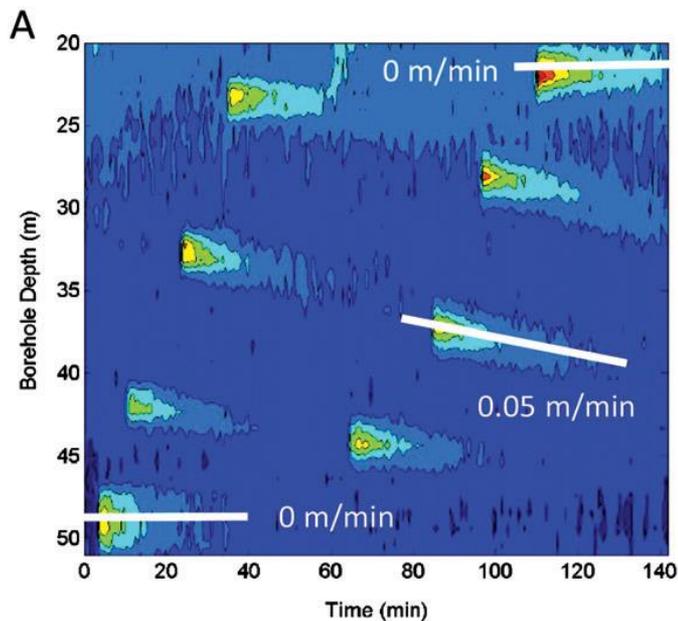
Fracture Flow Detection in Tuscola, IL, 2016-2017

Dolomite
+
Limestone



3. Current and Future Related Projects

Fracture Flow Detection in Madison, WI, 2013



Fiber-Optic Distributed Temperature Sensing (FO-DTS)

Strengths:

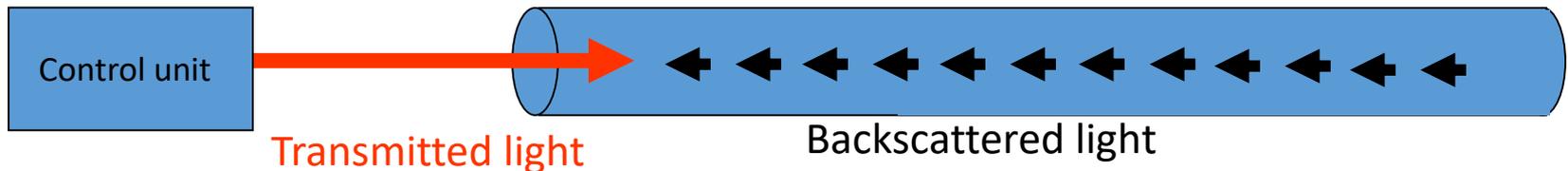
- High spatial resolution (~0.5 to 1 m)
- High precision (0.01° C)
- Large scale (10's of km possible)
- Continuous measurement (in time and space)
- Continuous data download (no retrieval/disturbance)
- Long-term installation possible
- Mobility

Limitations:

- Fiber is glass – can be damaged
- Deployment can be labor-intensive
- DTS systems are costly (\$15-100K) but getting cheaper
- Require calibration and field verification with conventional measurements



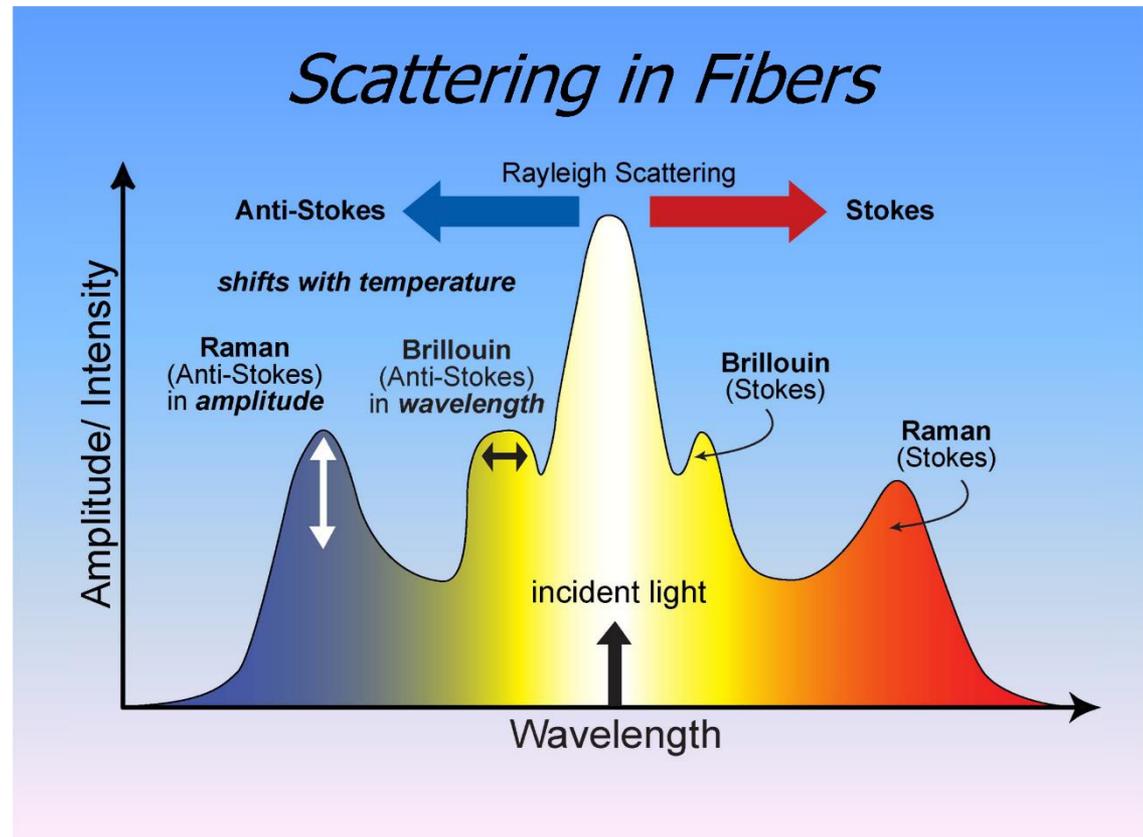
Measurement Physics (1/3)



- Control unit transmits laser light down cable
- Cable acts as a “light pipe”
- Light scatters back to the control unit by several mechanisms (Rayleigh, Brillouin, Raman)

Measurement Physics (2/3)

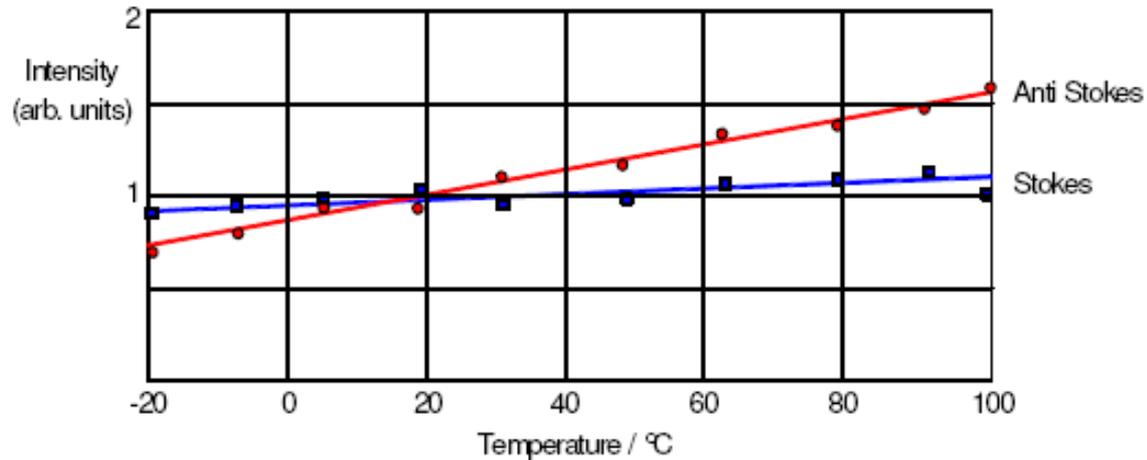
- **Rayleigh scatter** –frequency of incident light
- **Raman** (scatter a function of electron vibrational state): Intensity of anti-stokes depends on temperature
- **Brillouin** (scatter from variations in glass density): Wavelength of anti-stokes depends on temperature (intensity depends on strain)



From NSF-CTEMPs

Measurement Physics (3/3)

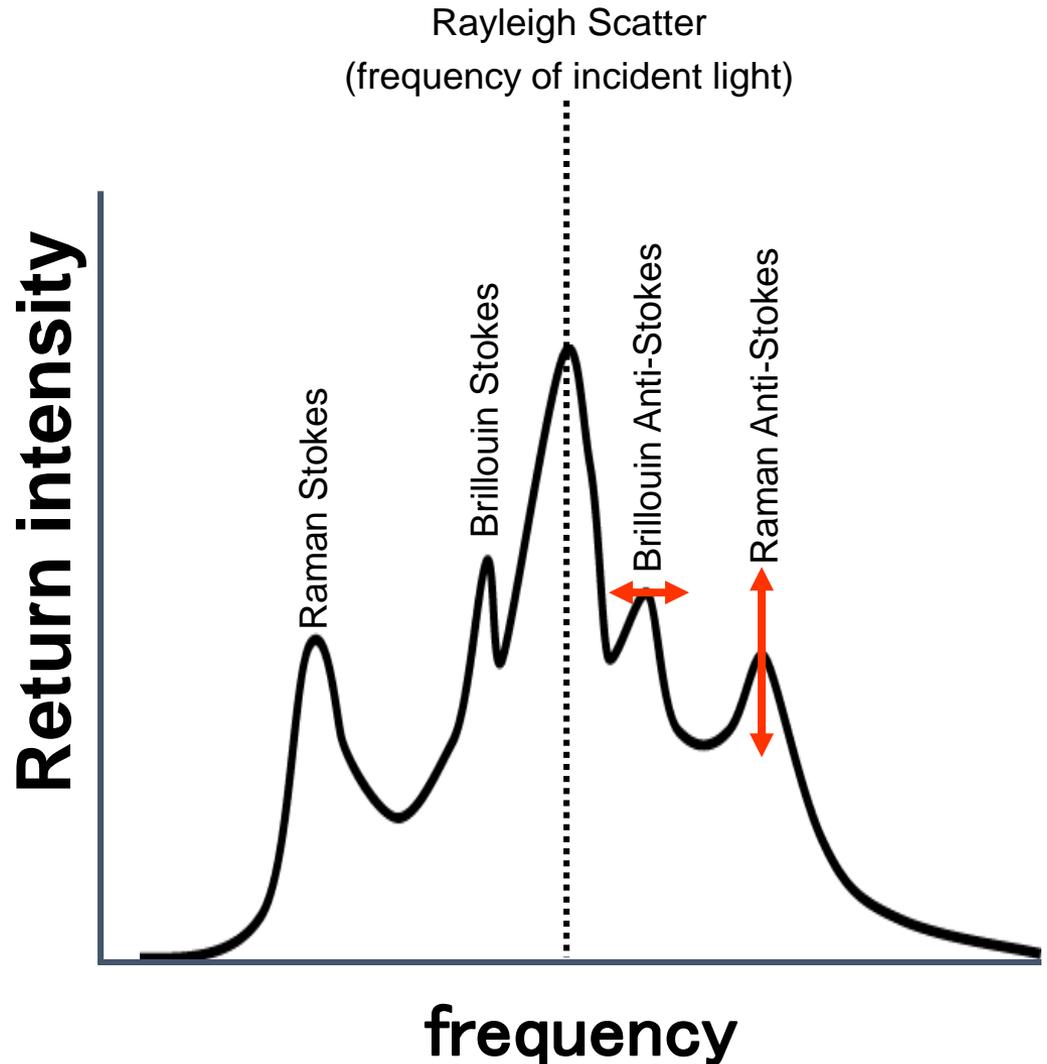
- Raman anti-stokes is highly sensitive to temperature
- Raman stokes is less sensitive
- Measurement principle: Infer temperature from ratio of Stokes:Anti-stokes



From Lios Operating Manual

Measurement physics

- **Rayleigh scatter** –frequency of incident light
- **Raman** (scatter a function of electron vibrational state): Intensity of anti-stokes depends on temperature
- **Brillouin** (scatter from variations in glass density): Wavelength of anti-stokes depends on temperature (intensity depends on strain)



Measurement physics

Raman-based DTS – going from backscatter to temperature (See PDF of Lee LFW article)

$$R(T) = \frac{I_{stokes}}{I_{anti-stokes}} = \left(\frac{\lambda_{stokes}}{\lambda_{anti-stokes}} \right)^4 \exp\left(-\frac{hc\nu'}{kT} \right)$$

Where,

- $\lambda_{anti-stokes}$ and λ_{stokes} are the anti-stokes and stokes wavelengths
- ν' the wavenumber separation from the pump wave length
- h is Planck's constant
- c is the velocity of light
- k is the Boltzman constant
- T is the absolute temperature of the fiber core

Measurement physics

Calculating absolute temperature at a location (See PDF of Lee LFW article)

$$T = \left[\frac{1}{\theta} - \frac{k}{hcv'} \ln \left(-\frac{R(T)}{R(\theta)} \right) \right]$$

Where,

- θ is the temperature for a reference section of fiber
- $R(\theta)$ is the intensity ratio (Stokes/Anti-stokes) for the reference section of fiber

Notes:

- Instruments have software to do all of this work for you
- May have to calibrate measurements outside software – need for conventional measurements
- Instrument output (options): Stokes, Antistokes, temperature